

## The utilization of the Taguchi method on microring resonator design parameters to enhance the value of the quality factor

Ahmad Aminudin<sup>1</sup>, Lilik Hasanah<sup>1</sup>, Harbi Setyo Nugroho<sup>1</sup>, Chandra Wulandari<sup>1</sup>, Budi Mulyanti<sup>2</sup>,  
Roer Eka Pawinanto<sup>3</sup>, Ahmad Rifqi Md Zain<sup>4</sup>, Gandi Sugandi<sup>5</sup>, Ida Hamidah<sup>6</sup>, Widyaningrum  
Indrasari<sup>7</sup>, Jumril Yunas<sup>4</sup>

<sup>1</sup>Physics Study Program, Faculty of Mathematics and Natural Science Education, Universitas Pendidikan Indonesia, Bandung, Indonesia

<sup>2</sup>Electrical Engineering Study Program, Faculty of Engineering Education and Industry, Universitas Pendidikan Indonesia, Bandung, Indonesia

<sup>3</sup>Industrial Automation Engineering Education and Robotics Study Program, Faculty of Engineering Education and Industry, Universitas Pendidikan Indonesia, Bandung, Indonesia

<sup>4</sup>Institute of Microengineering and Nanoelectronics, Universiti Kebangsaan Malaysia, Bangi, Malaysia

<sup>5</sup>Sensor and Actuator Devices Research Group, National Research and Innovation Agency, Bandung, Indonesia

<sup>6</sup>Automotive Engineering Education Study Program, Faculty of Engineering and Industrial Education, Universitas Pendidikan Indonesia, Bandung, Indonesia

<sup>7</sup>Physics Study Program, Faculty of Mathematics and Natural Science, Universitas Negeri Jakarta, Jakarta, Indonesia

### Article Info

#### Article history:

Received Dec 24, 2024

Revised Aug 9, 2025

Accepted Sep 1, 2025

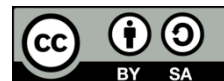
#### Keywords:

Design of experiments  
Finite difference time domain  
simulation  
Microring resonator  
Photonic sensors  
Quality factor optimization  
Refractive index sensing  
Taguchi method

### ABSTRACT

This study uses the Taguchi method to optimize the quality factor (Q-factor) of microring resonators (MRRs) for sensor applications. The MRRs are compact optical components widely used in biosensors and environmental monitoring due to their sensitivity to refractive index changes. The Q-factor, a key performance metric for MRRs, is significantly influenced by structural parameters such as ring radius (R), gap (g), waveguide width (W), and waveguide height (h). We employed a finite difference time domain (FDTD) simulation to model light propagation within the MRR and compute the corresponding Q-factor to identify the optimal combination of these parameters. An L9 orthogonal array (OA) is used in the Taguchi method to analyze each factor's influence with three levels systematically. The optimization resulted in a Q-factor of 6208.44, significantly higher than the baseline value, indicating a substantial improvement. Compared to previous works, this research highlights the advantages of combining FDTD-based electromagnetic modeling with statistical optimization, offering a structured yet efficient approach to MRR design. The proposed method enhances Q-factor performance and provides scalability for practical applications in biomedical and environmental sensing. These findings underscore the utility of Taguchi-based design in advancing the field of photonic sensor optimization.

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### Corresponding Author:

Roer Eka Pawinanto

Industrial Automation Engineering Education and Robotics Study Program

Faculty of Engineering Education and Industry, Universitas Pendidikan Indonesia

Dr. Setiabudi Road No.229, Isola, Sukasari, Bandung, West Java 40154, Indonesia

Email: roer\_eka@upi.edu

## 1. INTRODUCTION

Microring resonator (MRR) is a photonic-based device that utilizes light interference within MRR waveguides [1]. In the last decade, MRRs have been developed for sensor applications [2]. Light constructive interference is responsible for producing the resonance of MRR, which can be further examined to analyze

the works of MRR-based sensors. The investigated MRR is configured as an add-drop system consisting of two straight waveguides and a single-ring waveguide, as shown in Figure 1. This configuration allows MRR to have better characteristics, such as being more reflective, having a more stable temperature, and having a narrower bandwidth [3]-[5]. The dimensions of MRR are illustrated clearly, including ring radius, gap, waveguide width, and waveguide height, which are denoted as  $R$ ,  $g$ ,  $w$ , and  $h$ , respectively.

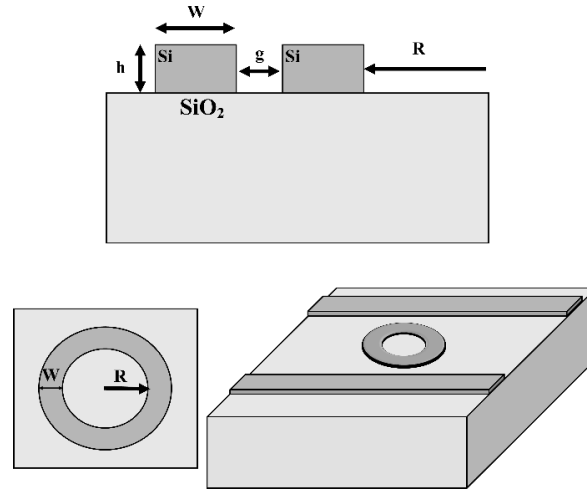


Figure 1. The illustration of a geometric MRR structure with a Si waveguide layer and a SiO<sub>2</sub> buffer layer

The performance of MRR is greatly determined by the size of each dimension and the material used, as light propagation in MRR depends on those parts [6]-[9]. The substrate and waveguide materials used are based on SiO<sub>2</sub> and Si, respectively, due to their outstanding optical properties and excellence as wave-guiding materials [10], [11]. In the case of MRR applications as sensors, quality factors (Q-factor) determine the detection capability of an MRR-based sensor that operates on a shift resonance scheme [12], [13]. A sharper resonance distinguishes a smaller resonance shift from a higher Q-factor [14]. This results in a lower detection limit, making the sensors more sensitive. The Q-factor is mainly described as the ratio between the resonance wavelength  $\lambda_o$  and the full width at half maximum (FWHM) [15], [16]. The value of the Q-factor greatly depends on the geometrical structure, such as the group index  $n_g$  and round-trip length  $L$  of MRR, as shown in (1).

$$Q = \frac{\lambda_o}{FWHM} = \frac{\pi n_g L}{\lambda \cos^{-1}(\psi)} \quad (1)$$

We employed the Taguchi method for further robust optimization to choose the best possible combination of the geometrical dimensions of MRR. Compared to other robust optimization methods such as stability radius, minimax estimator, stochastic optimization, and info-gap decision theory. The Taguchi method provides excellence, including a specific loss function, the philosophy of off-line quality control, and innovation in the design experiments [17], [18]. On the other hand, the different methods, such as Box-Behnken and Plackett-Burman, have main drawbacks, which only require that factors be varied in three factors, and the two-factor interactions cannot be studied [19], [20]. Consequently, the excellent parameter investigation technique in the experiment led to an improvement in the manufactured quality. Hence, the solution to improve device performance can be obtained through the Taguchi method because the control factors that have the most significant impact on optimization are directly involved in the analysis process of this method.

Theoretical work using the finite difference time domain (FDTD) method was generally used to investigate wave propagation through a medium or space within the time domain framework [21]-[23]. The analysis process with the FDTD method involves discrete light propagation in the waveguide, a continuous physical phenomenon. Discretization is carried out in Maxwell's time-dependent differential equation using a central-difference approach so that the differential equations for  $\vec{H}$  and  $\vec{E}$  are obtained explicitly, as shown in (2)-(7) [24]. The solution for  $\vec{H}$  can be obtained by solving the differential equation component of the electric field vector in a space for a specific time. In contrast, the solution for  $\vec{E}$  can be obtained by solving the magnetic field vector differential equation component in a space equal to the electric field vector component for a specific time after that. Hence, by framing these  $\vec{H}$  and  $\vec{E}$  solutions, the propagating light through the MRR waveguide can be investigated using the FDTD method.

$$\frac{\partial E_z}{\partial y} - \frac{\partial E_y}{\partial z} = -\frac{\mu_{xx}}{c_0} \frac{\partial \tilde{H}_x}{\partial t} \quad (2)$$

$$\frac{\partial E_x}{\partial z} - \frac{\partial E_z}{\partial x} = -\frac{\mu_{yy}}{c_0} \frac{\partial \tilde{H}_y}{\partial t} \quad (3)$$

$$\frac{\partial E_y}{\partial x} - \frac{\partial E_x}{\partial y} = -\frac{\mu_{zz}}{c_0} \frac{\partial \tilde{H}_z}{\partial t} \quad (4)$$

$$\frac{\partial \tilde{H}_z}{\partial y} - \frac{\partial \tilde{H}_y}{\partial z} = -\frac{\varepsilon_{xx}}{c_0} \frac{\partial E_x}{\partial t} \quad (5)$$

$$\frac{\partial \tilde{H}_x}{\partial z} - \frac{\partial \tilde{H}_z}{\partial x} = -\frac{\varepsilon_{yy}}{c_0} \frac{\partial E_y}{\partial t} \quad (6)$$

$$\frac{\partial \tilde{H}_y}{\partial x} - \frac{\partial \tilde{H}_x}{\partial y} = -\frac{\varepsilon_{zz}}{c_0} \frac{\partial E_z}{\partial t} \quad (7)$$

In this work, we combine theoretical work using the FDTD method and a robust optimization process using the Taguchi method for MRR design optimization. This work aims to obtain the highest possible Q-factor by combining the various input parameters. The input parameter variation was chosen based on our literature study from several references, which considered MRR geometry and application for sensors. Further discussion will address how to implement the Taguchi method for optimizing MRR.

## 2. METHOD

### 2.1. Microring resonator design and modelling

The simulation of the MRR was conducted using the 3-dimensional FDTD (3D FDTD) method via Lumerical FDTD Solutions®. The FDTD technique solves time-dependent Maxwell's equations—a set of partial differential (2)–(7)—to describe the behavior of electromagnetic fields in space and time. This numerical method is highly effective in simulating the light propagation and field distribution in photonic devices such as MRRs.

An MRR is an integrated optical device consisting of a circular waveguide (the ring) that couples light from straight waveguides positioned nearby. Due to its sensitivity to changes in effective refractive index, it is widely used in optical sensing, filtering, and wavelength multiplexing applications. MRRs detect environmental changes in sensor configurations by observing resonance shifts or variations in their Q-factor.

Figure 2 illustrates the MRR model constructed in Lumerical FDTD Solutions®. The simulation began with creating the base structure, including the buffer layer and the waveguides. The buffer layer was defined using a rectangular geometry from the “structure” menu, while the MRR was formed by selecting the “ring resonator” component under “integrated optics”. The design factors studied in this research are the ring's geometric parameters—ring radius, gap between waveguides, waveguide width, and waveguide height, as shown in Figure 2. These parameters directly affect the mode confinement and resonance behavior of the MRR.

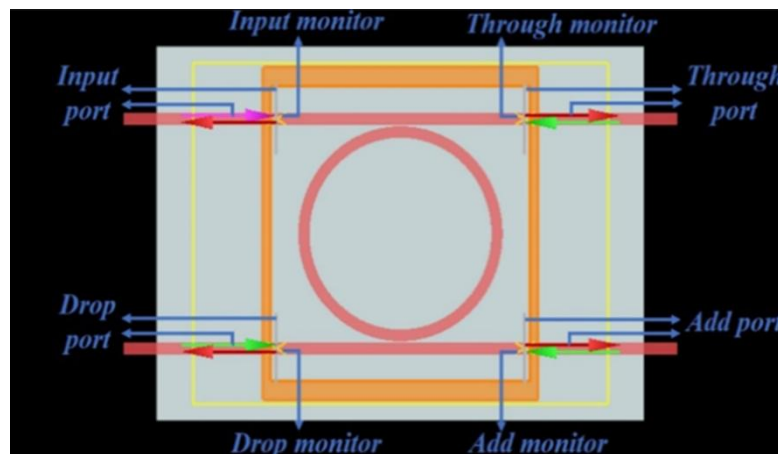


Figure 2. Geometric model of MRRs using FDTD Solutions®

After defining the structure, port objects and time-domain monitors were placed at four locations: the input port, through port, drop port, and add port. Ports define the optical signal's entry and exit points and allow control over the mode, frequency range, and polarization. The time-domain monitors record electromagnetic field data during the simulation, enabling post-processing in both the time and frequency domains.

A Gaussian optical pulse was launched into the input port. The simulation time was set to 50,000 fs, sufficient for the optical signal to traverse the domain completely and interact with the resonator. This duration ensures that resonance and ring-down phenomena are fully captured. The simulation was carried out in an ambient environment at a temperature of 295 K and air refractive index  $n=1$ , approximating experimental laboratory conditions.

The simulation engine discretized the spatial region into a Yee cell lattice, calculating the electric and magnetic field components at every point. After completing the simulation, the transmittance at the through port was plotted. Resonance appears as dips in the transmittance spectrum at certain wavelengths. The FWHM was extracted from these data to compute the Q-factor, a dimensionless parameter that describes resonance sharpness and is crucial for sensor sensitivity.

## 2.2. Taguchi method for microring resonator design

The goal of this research is to enhance the performance of the MRR by maximizing its Q-factor. To achieve this, the Taguchi method was employed. Developed by Genichi Taguchi, this statistical approach improves quality and performance in product design and engineering by minimizing variability and identifying optimal parameter settings [25]-[27]. Figure 3 shows the processes involved in MRR optimization using the Taguchi method.

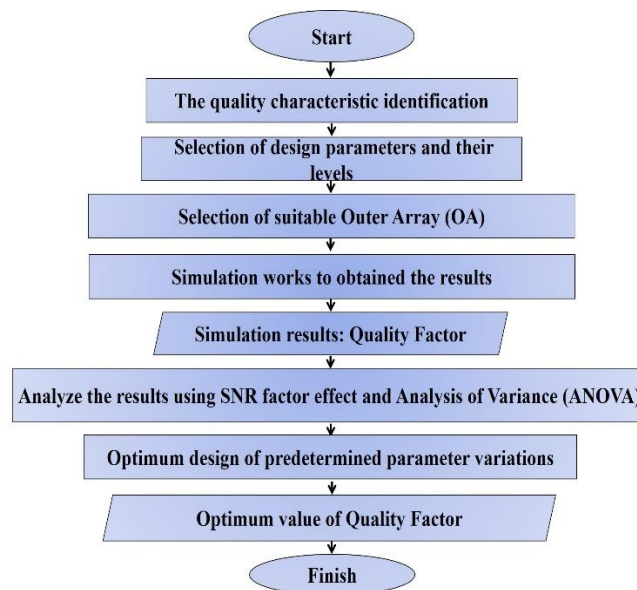


Figure 3. The Taguchi method flow diagram for MRR optimization

The Taguchi method begins with identifying the quality characteristic to be optimized—in this case, the Q-factor, as it directly influences the sensitivity and effectiveness of the MRR in sensing applications [28], [29]. Once the quality target is set, the next step involves selecting design parameters (control factors) and assigning levels to each. These factors significantly influence the resonator's behavior. Based on literature review and sensitivity analysis [30], [31], four control factors were chosen: ring radius, gap, waveguide width, and waveguide height. Each factor was tested at three levels, as shown in Table 1.

Table 1. Control factor for the design and simulation of MRRs

Symbol	Control factor	Unit	Level 1	Level 2	Level 3
R	Ring radius	$\mu\text{m}$	4.00	4.50	5.00
g	Gap	$\mu\text{m}$	0.09	0.12	0.15
W	Waveguide width	$\mu\text{m}$	0.45	0.46	0.47
h	Waveguide height	$\mu\text{m}$	0.14	0.16	0.18

To efficiently explore the parameter space while minimizing simulation runs, the L9 orthogonal array (OA) was selected. This OA is widely used when dealing with 4 factors at 3 levels, as it reduces the number of experiments from 81 ( $3^4$ ) to just 9, while still allowing interaction analysis and optimization. Each of the 9 combinations defined by the L9 OA was simulated using the same FDTD setup described in subsection 2.1. The Q-factor obtained from each simulation was then used to compute the signal-to-noise ratio (SNR) using the "larger-the-better" criterion, which is suitable for maximization goals [32].

$$\text{SNR} = -10 \log_{10} \frac{1}{n} \sum_{i=1}^n \left( \frac{1}{y_i^2} \right) \quad (8)$$

$n$  is the number of simulations performed, and  $y_i$  is the value of the Q-factor obtained in each simulation. The SNR values help determine which factor levels lead to a more robust and higher Q-factor. After calculating the SNRs, an analysis of variance (ANOVA) was performed to assess the relative impact of each design factor on the Q-factor. The most influential parameters were identified by comparing each control factor's average SNR values at different levels. This process enabled the identification of the optimal combination of MRR design parameters, maximizing the Q-factor and enhancing device performance for practical sensor applications.

### 3. RESULTS AND DISCUSSION

The L9 OA was the outer array, ideal for evaluating four control factors at three levels. This setup generates nine combinations of the control factors, as presented in Table 2. The Q-factor and SNR values used for optimization in this study were derived from these nine configurations. The SNR calculation follows the "larger-is-better" formulation commonly used in Taguchi optimization for quality improvement.

Table 2. The SNR value of the arrangement is orthogonal L9

Sim.	R	g	W	h	Q	SNR
1	1	1	1	1	644.61	56.19
2	1	2	2	2	2059.64	66.28
3	1	3	3	3	5226.40	74.36
4	2	1	2	3	2556.16	68.15
5	2	2	3	1	1295.65	62.25
6	2	3	1	2	2963.53	69.44
7	3	1	3	2	1556.31	63.84
8	3	2	1	3	2895.35	69.23
9	3	3	2	1	1558.28	63.85

The primary objective of this study is to determine the most influential design parameters for the Q-factor of the MRR. The Taguchi method provides a systematic and statistically efficient approach for optimizing multiple parameters with a minimal number of experiments. By employing the "larger-is-better" SNR criterion, we can quantify the contribution of each control factor variation to the observed Q-factor performance. Table 2 shows that variations in control factors lead to considerable differences in the resulting Q-factor and SNR values. A preliminary examination suggests that some factors significantly influence the performance, necessitating a quantitative analysis. The ANOVA and SNR response tables are used to identify the magnitude of each factor's impact.

The performance sensitivity of each factor is evaluated by the  $\Delta$  value, which is the difference between the highest and lowest SNR across the levels. A larger  $\Delta$  indicates a more influential control factor. Based on Table 3, waveguide height and gap exhibit the most pronounced effects on the Q-factor, with  $\Delta$  values of 9.82 and 6.49, respectively. These results imply that fine-tuning the vertical geometry of the waveguide and the gap distance between the ring and the bus waveguide significantly improves the resonator's performance. In contrast, the ring radius and waveguide width show relatively modest impact, with  $\Delta$  values of 1.00 and 1.87, respectively. This finding differs from initial assumptions and highlights the necessity of quantitative evaluation via SNR and ANOVA, rather than relying solely on theoretical intuition.

Table 3. The SNR response for the Q-factor

Symbol	Control factor	SNR			$\Delta$
		Level 1	Level 2	Level 3	
R	Ring radius	65.61	66.61	65.64	1.00
g	Gap	62.73	65.92	69.22	6.49
W	Waveguide width	64.95	66.09	66.82	1.87
h	Waveguide height	60.76	66.52	70.58	9.82

The SNR response analysis results are visualized in Figures 4(a) to (d), graphically illustrating how each control factor level influences the SNR. The optimal levels for each factor can be deduced directly from the highest points in each subfigure of the plot. The optimal value for the ring radius is at level 2, which is  $R=4.5\ \mu\text{m}$ . The optimal value for the waveguide gap factor is at level 3, namely  $g=0.15\ \mu\text{m}$ . The optimal value for the waveguide width is at level 3, namely  $W=0.47\ \mu\text{m}$ . The optimal value for the waveguide height is at level 3, namely  $h=0.18\ \mu\text{m}$ .

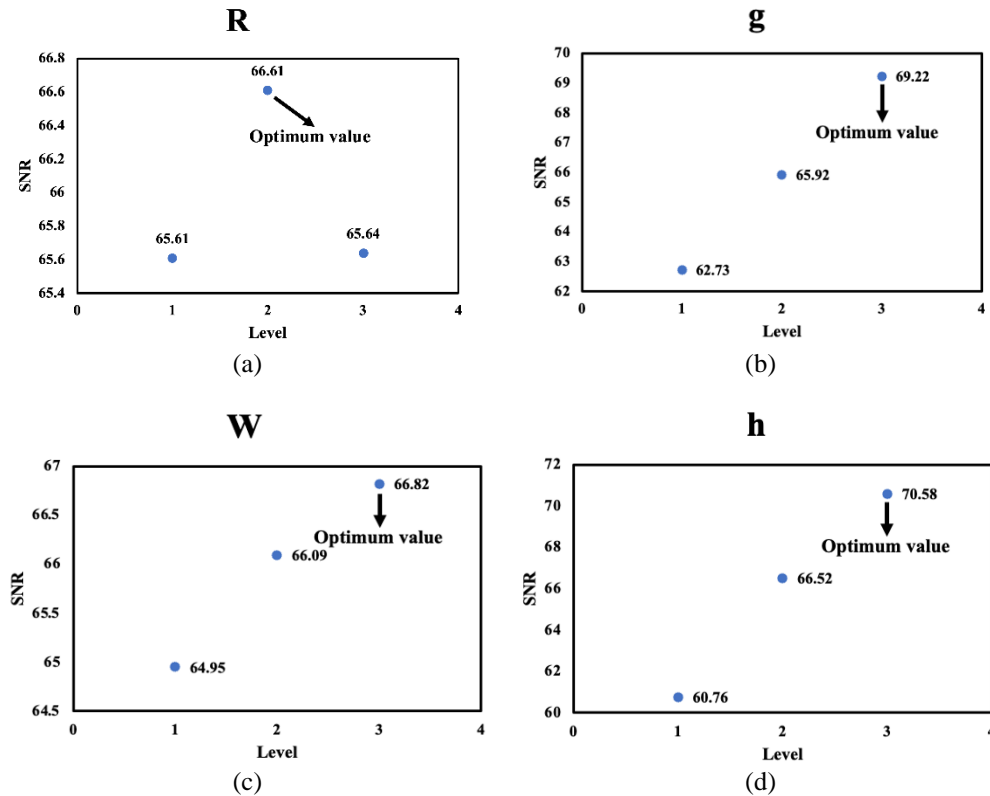


Figure 4. The optimal SNR response for Q-factors according to the four different control factors, namely; (a) ring radius, (b) gap, (c) waveguide width, and (d) waveguide height

While the current study successfully applies the Taguchi method for optimization, future work could validate these optimal settings through additional experiments or simulations and compare results to those reported in existing literature to articulate the contribution and novelty more clearly. Nevertheless, within the constraints of this study, the method effectively isolates the most impactful parameters, particularly waveguide height and gap, in enhancing MRR performance. To improve the discussion of results, a comparison with existing work could be made to highlight the novelty of the obtained results. The optimization result shows a higher Q-factor value than the pre-optimization result in Table 4.

Table 4. Q-factor optimization results using the Taguchi method

Optimum factor control				Optimum Q-factor
R ( $\mu\text{m}$ )	g ( $\mu\text{m}$ )	W ( $\mu\text{m}$ )	h ( $\mu\text{m}$ )	
4.50	0.15	0.47	0.18	6208.44

#### 4. CONCLUSION

This study demonstrates the use of the Taguchi method in optimizing the design parameters of an MRR to enhance its Q-factor, which is crucial for sensor performance. The study identified the most influential factors and optimal design configuration by systematically analyzing four geometric parameters—ring radius, gap, waveguide width, and waveguide height—through a  $3 \times 4$  L9 OA.

The SNR analysis and response table revealed that waveguide height and gap significantly impact the Q-factor, with  $\Delta$  values of 9.82 and 6.49, respectively. The Taguchi method enabled a data-efficient yet

reliable prediction of the optimal parameter combination, achieving an estimated Q-factor of 6208.44 substantially higher than the initial configurations. These findings underscore the value of Taguchi-based statistical design of experiments (DOE) in photonic device optimization.

Although the optimization result is theoretical and not experimentally verified due to simulation constraints, the methodology provides a robust framework for guiding future experimental validation and device fabrication. Compared to traditional trial-and-error or full-factorial methods, the Taguchi approach offers a more structured and resource-efficient route for performance improvement in photonic sensor design. This study contributes to the ongoing development of high-performance optical resonators and supports adopting design optimization techniques in integrated photonics research.

FUNDING INFORMATION

We gratefully acknowledge Lembaga Penelitian Dan Pengabdian Kepada Masyarakat Universitas Pendidikan Indonesia for financial support through the Penelitian Kerjasama Internasional No 337/UN40 grant.LP/PT.01.03/2024.

AUTHOR CONTRIBUTIONS STATEMENT

This journal uses the Contributor Roles Taxonomy (CRediT) to recognize individual author contributions, reduce authorship disputes, and facilitate collaboration.

Name of Author	C	M	So	Va	Fo	I	R	D	O	E	Vi	Su	P	Fu
Ahmad Aminudin				✓	✓					✓				
Lilik Hasanah	✓									✓		✓		✓
Harbi Setyo Nugroho						✓		✓	✓		✓			
Chandra Wulandari		✓						✓	✓				✓	
Budi Mulyanti					✓		✓			✓		✓		
Roer Eka Pawinanto	✓	✓			✓					✓				
Ahmad Rifqi Md Zain		✓	✓							✓				
Gandi Sugandi					✓	✓				✓				
Ida Hamidah					✓		✓			✓				
Widyaningrum					✓					✓				
Indrasari														
Jumril Yunas			✓	✓	✓					✓				

- C : **C**onceptualization  
M : **M**ethodology  
So : **S**oftware  
Va : **V**alidation  
Fo : **F**ormal analysis
- I : **I**nterpretation  
R : **R**esources  
D : **D**ata Curation  
O : **O**riginal Draft  
E : **E**diting
- Vi : **V**isualization  
Su : **S**upervision  
P : **P**roject administration  
Fu : **F**unding acquisition

CONFLICT OF INTEREST STATEMENT

The authors declare that they have no known competing financial interests.

INFORMED CONSENT

We have obtained informed consent from all individuals included in this study.

ETHICAL APPROVAL

There is no ethical approval needed since there is no experiment or data related to human or animal used.

DATA AVAILABILITY

Data availability is not applicable to this paper as no new data were created or analyzed in this study.

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## BIOGRAPHIES OF AUTHORS






**Ahmad Aminudin**    in 1992, was admitted to the Department of Physics at the University of Indonesia (UI). He graduated with a Bachelor's degree in 1998. In 1999, he continued his Master's degree in the same field and completed it in 2004. In 2003, he was accepted as a Lecturer in the Department of Physics at the Bogor Agricultural University (IPB). In 2008, he was appointed as a Lecturer in the Department of Physics Education at the Faculty of Mathematics and Natural Sciences, Universitas Pendidikan Indonesia (UPI), and became a civil servant. In 2011, he pursued a Doctoral study in the Physics Department at the Bandung Institute of Technology (ITB), specializing in Instrumentation Physics, and received a scholarship from the Directorate General of Higher Education (DIKTI). Since 2003, his research focus has been in the fields of sensors and transducers, measurement systems, instrumentation systems, control systems, and applied physics. He has been involved in numerous research projects in collaboration with various research institutes, including the National Research and Innovation Agency (BRIN), the Department of Physics at Bogor Agricultural University, the Department of Physics at the University of Indonesia, and the Department of Physics at the Bandung Institute of Technology (ITB). He has produced 90 publications to date, including both national and international scientific papers. His research has earned an h-index of 6 on Scopus and an h-index of 8 on Google Scholar, with a total of 263 citations. He can be contacted at email: aaminudin@upi.edu.






**Lilik Hasanah**    was born in Purworejo on June 16, 1977. In 1995, she was admitted to the Department of Physics at Institut Teknologi Bandung (ITB) and graduated in 1999. She continued her studies for a Master's degree in the same department at ITB, completing it in 2001. In 2001, she became a lecturer in the Physics Education Department at FPMIPA, Universitas Pendidikan Indonesia (UPI), and was appointed a civil servant. In 2003, she pursued a Ph.D. in the Department of Physics at ITB, specializing in Computational Physics of Electronic Materials, supported by a scholarship from The Habibie Center Foundation. From 2009 to 2010, she participated in the DIKTI Academic Recharging Program, conducting collaborative research at the Department of Semiconductor Electronics and Integration Science, Graduate School of Advanced Sciences of Matter, Hiroshima University, Japan. Since 2008, she has been actively involved in numerous research collaborations with institutions nationally and internationally. These include BRIN (National Research and Innovation Agency), NCI, Hiroshima University, the Institute of Microengineering and Nanoelectronics (IMEN) at Universiti Kebangsaan Malaysia (UKM), the Department of Mechanical Engineering at Universiti Malaysia Pahang, the Faculty of Engineering at Universiti Malaysia Sarawak, the National University of Singapore (NUS), and many others. To date, she has produced 140 publications, encompassing national and international scientific works, with a Scopus h-index of 10 and a Google Scholar h-index of 14, accumulating 463 citations. She can be contacted at email: lilikhasanah@upi.edu.






**Harbi Setyo Nugroho**    received his Bachelor's degree in Physics from Universitas Pendidikan Indonesia in 2019, where his research focused on silicon-on-insulator microring resonators for glucose detection. He completed his Master's degree in Engineering Physics at Institut Teknologi Bandung in 2021, with a thesis on the influence of synthesis process modification and sulfurization on the growth of CZTS thin-film crystal layers. His academic interests include thin-film photovoltaics, photonic sensing, and material characterization. He can be contacted at email: harbisn5@gmail.com.






**Chandra Wulandari**    is a Doctoral student in Engineering Physics and a research member at the Advanced Functional Materials Laboratory, Institut Teknologi Bandung (ITB). She earned her master's degree in Engineering Physics from ITB in 2022. Over the past five years, her research has focused on the development of biosensors, including optical- and electrochemical-based approaches. For her master's thesis, she successfully developed surface plasmon resonance-based biosensors utilizing the 2D material MoS<sub>2</sub>. She is currently working on the development of porous materials for high-performance electrochemical biosensors and has been conducting visiting research at the National Institute of Materials Science (NIMS), Japan, for one year to support her doctoral work. In addition, since 2020, she has been involved as a research assistant at the Indonesian University of Education, contributing to research in the field of materials. She can be contacted at email: 33322303@mahasiswa.itb.ac.id






**Budi Mulyanti**    is a professor of material physics at the Faculty of Engineering and Industrial Education (FPTI), Universitas Pendidikan Indonesia (UPI). She received Ph.D. in physics from Institut Teknologi Bandung, Indonesia in 2006. She is a senior member of the Institution of Electrical and Electronics Engineer (IEEE) since 2022. She is also a vice chairman of physics society of Indonesia, Bandung Chapter. She is a member of National Credit Assessment Team of Republic of Indonesia and also member of National Research Reviewer Republic of Indonesia. She was a head of the Department of Electrical Engineering and Education FPTK UPI from 2015 until 2019. She was also head of TVET center FPTK UPI from 2008 until 2010. She was awarded as the best researcher from Universitas Pendidikan Indonesia in 2016. She has published three text books in material electronics for undergraduate courses and more than 80 academic research papers. Her interests are design and fabrication of photonic devices, bioMEMS, and solar cell development. She can be contacted at email: bmulyanti@upi.edu.







**Roer Eka Pawinanto**    is a senior lecturer at Universitas Pendidikan Indonesia. He received his Ph.D. in Electrical Engineering from Universiti Teknologi Malaysia under the Japan-ASEAN Integration Fund scholarship in 2020. He was awarded as Top 10 of UPI's most productive researcher in the SCOPUS-based publication and Top 10 Hackathon [RE] energize Indonesia from UPI and New Energy Nexus Indonesia, respectively, in 2020. In addition, he was awarded as a top 10 IEEE Innovation Nation Indonesia in 2021. He has published two book chapters in the electronics field and more than 50 academic research papers. His work focuses on MEMS devices and technology for sensors and actuators, energy, and biomedical applications. He can be contacted at email: roer\_eka@upi.edu.







**Ahmad Rifqi Md Zain**    is Associate professor of Electronics engineering at Institute of Microengineering and Nanoelectronics (IMEN), Universiti Kebangsaan Malaysia (UKM). He received his degree and masters degree from Coventry University and Glasgow university, United Kingdom in 2002 and 2005 respectively. He also worked with Marconi Communication as hardware engineer United Kingdom from 2002-2004 before pursuing his study at Glasgow university. In 2009, He received his PhD from Glasgow University, United kingdom (with Prof Richard De La Rue), in Electronics engineering (1D photonic crystal cavities). After completing his postdoctoral studies in 2012 at Bristol university in Gallium nitride based optical biosensors (with Prof Martin J. Cryan), he joined IMEN, UKM in August, 2014. In 2017, he joined Prof Marko Loncar at School of engineering and applied sciences (SEAS), Harvard University as postdoctoral research fellow in applied physics until 2019, working on Quantum information. He is expert in nanophotonics, optoelectronics and nanofabrication, and his current interest include optical imaging at infra-red region, 2D materials, optical based biosensors (including photonic crystal based waveguide, SERS, LSPR), 1D and 2D photonic crystals, optical MEMS sensors, environmental and agricultural based sensors (including water security and farming industry), integrated optics and nanofabrication. He is a member of Optical Society of America, IEEE, IET and SPIE. He has been awarded several research grants nationally and internationally. He can be contacted at email: rifqi@ukm.edu.my.







**Gandi Sugandi**     received the B.Eng. degree in Electrical Engineering from Universitas Jenderal Achmad Yani, Indonesia, in 2001, the M.Eng. degree in Electrical Engineering (Microelectronics) from Institut Teknologi Bandung (ITB), Indonesia, in 2005, and the Ph.D. degree in Microengineering and Nanoelectronics from the Institute of Microengineering and Nanoelectronics (IMEN), Universiti Kebangsaan Malaysia (UKM), in 2015. He has been with the Indonesian Institute of Sciences (LIPI) from 1985 to 2021 and has continued his research career at the National Research and Innovation Agency (BRIN) since 2021. His research interests include thick- and thin-film technology for electrochemical sensors, MEMS-based sensors and actuators, and smart sensor systems. He has been awarded several research grants nationally and is an active member of the Indonesian Researchers Association (PPI). He can be contacted at email: gand001@brin.go.id.







**Ida Hamidah**     is currently a professor of Physics at Universitas Pendidikan Indonesia. She completed her undergraduate and doctoral degrees in the same field, Physics. She earned her undergraduate degree (IKIP Bandung, 1992), a master's degree (ITB, 1999), and a doctoral degree (ITB, 2006). Her research interests are quite diverse, spanning materials physics, engineering, and science education. This is due to her role as both a scientist and a lecturer supervising student research. Specifically, her research topics include piezoelectricity, energy harvesting, and online learning; and research related to low-carbon education includes energy conservation, greenhouse gases, low-carbon transportation, and sustainable development. She can be contacted at email: idahamidah@upi.edu.



**Widyaningrum Indrasari**     received her Bachelor's degree in Physics from Institut Teknologi Bandung (ITB) in 1999 and her Master's degree in Physics from the same institution in 2005. In 2009, she continued her doctoral studies at the Department of Physics, ITB, and was awarded the Doctoral degree in 2014 with a specialization in Instrumentation Physics. Since 2006, she has been a faculty member at Universitas Negeri Jakarta (UNJ). Her research activities focus on the development of sensors for environmental monitoring systems and the enhancement of photovoltaic performance using maximum power point tracking (MPPT) and modified DC-DC converter circuits. She has been actively engaged in both teaching and research, with particular interest in applied physics and renewable energy systems. She can be contacted at email: widyaningrum-indrasari@unj.ac.id.



**Jumril Yunas**     is Assoc. Professor at the IMEN-UKM, Institute of Microengineering and Nanoelectronics, Universiti Kebangsaan Malaysia. He graduated in electrical engineering at the University of Technology RWTH Aachen, Germany and obtained his Ph.D. at the Universiti Kebangsaan Malaysia. He was Research Fellow at Indonesian Institute of Sciences, Indonesia and visiting scientist at the Chiba University, Japan. His work is focused on MEMS device and technology for sensors and actuators, energy, and biomedical applications. He can be contacted at email: jumrilyunas@ukm.edu.my.